Upstream Oil and Gas Emissions Calculations: Storage Tanks

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Upstream Oil and Gas Emissions Calculations: Storage Tanks

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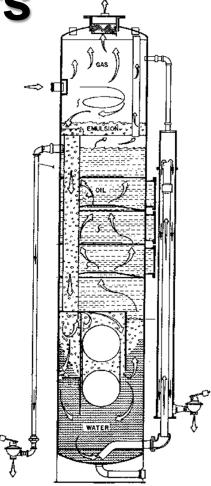
Overview

- Briefly review emissions calculations for separators
- Focus on emissions calculations for storage tanks, specifically use of Exploration and Production (E&P) TANK
- Use of sampling data



Analyzing Data and Determining Emissions: Separators

- Generally operate above ambient pressure
- May be uncontrolled, typically in oil field
- Flash emissions are a concern if uncontrolled
- Emissions determined using:
 - Process simulator
 - Measurement data (will be discussed in storage tanks portion of presentation)



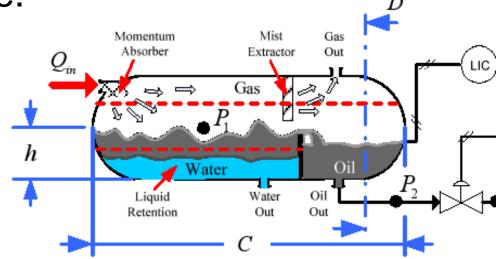


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Analyzing Data and Determining Emissions: Separators (cont.)

- Even if separator is controlled, last stage separator will have direct impact on storage tank emissions.
- Determine whether last stage separator is twophase or three-phase.
- Obtain actual separator pressure and temperature to use for calculation inputs.





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Analyzing Data and Determining Emissions: Separators (cont.)

For process simulator, inputs may include:

- Operating temperatures and pressures of the various process vessels at the facility
- Composition of the inlet gas
- Gas flow rate off the inlet separator
- Composition of the final stabilized oil/condensate product from the stock tanks



- Oil and water production rates to the stock tanks
- API gravity of liquid(s)
- Molecular weights of liquid and/or gas streams



- Three routine emissions modes: flash, working, breathing
- Flash emissions are generally largest emissions
- Emissions determined using:
 - Direct measurement
 - Process simulator models**
 - E&P TANK program
 - Vasquez-Beggs or Rollins, McCain, and Creeger correlations, or software that uses these correlation equations (such as GRI-HAPCalc)**
 - Gas/oil ratio (GOR) method**
 - AP-42 Chapter 7 equations (e.g., TANK ESP, TANKS 4.09d)*
 - *=method estimates working and breathing loss emissions only
 - **= method estimates flash emissions only

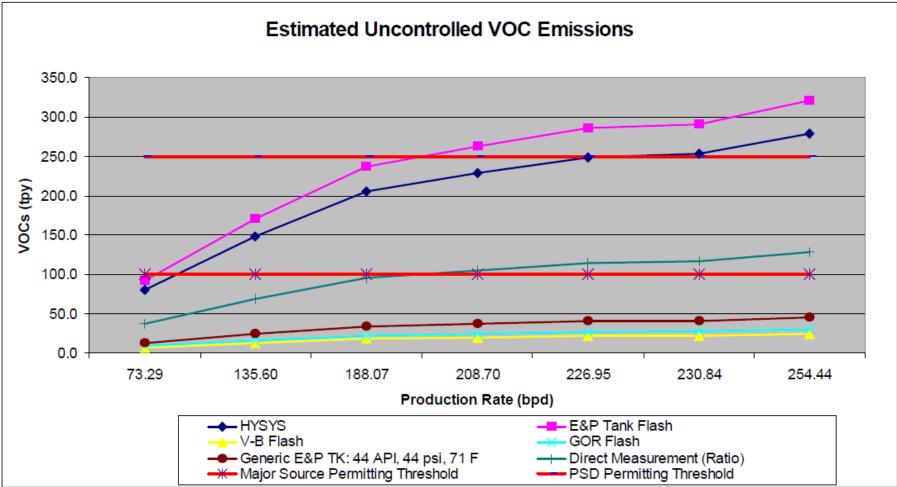


Table 1: Flash Loss Estimation Methods

| No. | Method | Emissions Calculated | Comments | |
|-------------------------------------|--|---------------------------------|--|--|
| 1 | Direct measurement of tank emissions | Working, Breathing, Flash | Sampling and analysis are expensive, but the results are relatively accurate.Sampling timing and duration are critical | |
| 2 | Process Simulator computer programs | Flash only | There are several different process simulators (e.g. WinSim, Designer II, HYSIM, HYSIS, VMG, and PROMAX, etc.). The software is expensive, but the results are accurate when based on site-specific sample and analysis . | |
| 3 | E&P Tanks Software, V 2.0, using an option that requires site-specific sampling | Working, Breathing, Flash | A pressurized liquid and/or gas sample analysis from a separator will be needed. This choice does not include the Geographical Data base option. | |
| 4 | Laboratory measurement of the Gas-Oil-Ratio (GOR) from a Pressurized Liquid Sample | Flash only | This is direct laboratory analysis of the flash gas emitted from a pressurized oil/condensate sample . | |
| 5 | Vasquez-Beggs Equation (VBE): | Flash only | A calculation method based on empirical data. The VBE variables must be supported with a lab sampling analysis that verifies the API gravity, separator gas gravity, stock tank gas molecular weight, and VOC fraction. If an operating variable used in the VBE calculations falls outside of the parameter limits, the applicant must use another method to calculate flash emissions. | |
| 6 | E&P Tanks Software, V 2.0, Geographical Database Option | Working, Breathing, Flash | Emissions are based on choosing an example case that closely matches operating parameters at the site in question. A justification for using this method must be included if the site is existing. The geographical database is based on 103 | |
| Not allowed for emissions inventory | | ventory | sampled sites and is a very poor estimate of emissions from any particular storage tank. | |
| 7 Not a | Griswold and Ambler GOR Chart Method Ilowed for emissions inv | Flash only /entory | A graph developed by Griswold and Ambler (1978) can be used to approximate total potential vapor emissions from a barrel of oil based on pressure differentials. The curves were constructed using empirical flash data from laboratory studies and field measurements. | |

Bakken Tank Flash VOC Emission Models and Direct Measurements





Source of data:

1) Comm Engineering, Vent Gas Direct Measurement and Sampling Report for Marathon Oil Company, July 21, 2009 (submitted to EPA July 31, 2009)

Direct measurement

- Two tests: one for flow rate, one for volatile organic compounds (VOC) concentration and speciation
- Should measure flash, working, and breathing losses
- Review test report critically
 - Ensure test period was at least 24 hours to capture full breathing loss cycle.
 - Review liquid levels pre- and post-test. If unchanged, then separator did not dump to tank and the test cannot be used to calculate flash and working loss emissions.
 - Will produce pound/hour or pound (lb)/barrel test result.
 - Pound per barrel is preferred since VOC emissions will increase with increased production.



 Example direct measurement calculations: use dimensional analysis to determine emissions.

| 12 lb <u>VOC</u> | Х | <u>28,000 barrel</u> | Х | ton = 168 tons VOC per year |
|------------------|---|----------------------|---|-----------------------------|
| barrel | | year | | 2000 lb |

- As long as liquid is present in the tank, emissions will be generated.
- If production ceased during the year, but the tank was not emptied, emissions will still need to be estimated.



- Determines flash, working, and breathing losses
- Models separator liquid transfer to tank to calculate flash emissions
- Requires gas and/or liquid sample analysis(es) along with operational data to run model
- Calculates working and breathing losses using either:
 - AP-42, Chapter 7 equations
 - Requires site-specific tank data inputs, typically more accurate
 - RVP option
 - Simulates a distillation column to arrive at sales 'oil' RVP



- Emissions driven by:
 - Stream composition
 - Separator pressure
 - Sales oil RVP
- First we'll discuss stream composition requirements, which depend upon sampling and related analysis.
- Obtaining an accurate gas or liquid sample analysis is critical: sample must be collected, stored, and analyzed properly.
- Samples are often collected for business purposes, but can be used for regulatory purposes if performed properly.



Regulatory and other goals of sampling:

- Determine amount of gas that will be flashed at the storage tank or potentially, the separator
- Can be used to determine GOR which can be used to calculate emissions



Regulatory and other goals of sampling, cont.:

- Determine VOC, acid gas, and hazardous air pollutants (HAP) or toxics composition data for gas and/or liquid phase
- Sales gas must meet pipeline specifications for transmission.



Gas composition analyses:

Almost all oil/gas process units require extended gas analysis to determine emissions accurately

HAPs present in trace amounts will not be detected in sales gas analysis.



- Gas composition analysis methods:
 - GPA Standard 2261: Analysis of Natural Gas and Similar Gaseous Mixtures

Does not provide extended analysis required to obtain HAP speciation.

 GPA Standard 2286: Analysis of Natural Gas and Similar Gaseous Mixtures by Temperature Programmed Gas Chromatography

Extended gas analysis, but does not provide nitrogen or carbon dioxide analysis.



Analyzing Data and Determining Emissions: Sample Analysis

Sampling analysis report: critical review

- Provide actual sample report, not Excel spreadsheet
- Review sample lab analysis:
 - Does the report state sample type (liquid, gas, mixture, etc.)?
 - Was the sample taken at that site?
 - If not, does it qualify as a representative sample?
 - Representative sample requirements:
 - Was the sample taken from the same geological formation or reservoir?
 - Is the sample processed and treated in the same manner at the sites in questions?
 - Is the API gravity within three degrees of the actual



Analyzing Data and Determining Emissions: Sample Analysis

Sampling analysis report: critical review (cont.)

Does the report state where at the site the sample was taken?

Important: samples may be required from different locations to accurately determine emissions for different process units.

- Was the initial opening pressure of the sample at the lab reported?
 - If so, it should be at or above separator pressure.
 - If not, leaks have occurred.



Analyzing Data and Determining Emissions: Sample Analysis

Sampling analysis report: critical review (cont.):

• Does the report state separator pressure and temperature?

If so, does it match operating conditions?

 Labs often perform quality control checks using a bubble point pressure test at the separator temperature.

The bubble point pressure should be comparable with the test separator pressure (within 30 pounds per square inch [psi] absolute).



Analyzing Data and Determining Emissions: Sample Analysis (cont.)

- Gas sample rules of thumb:
 - Low pressure separator gas is not representative of sales gas.
 - The VOC content of sales gas should be ~5 to 25 weight percent.



Analyzing Data and Determining Emissions: Sample Analysis (cont.)

- Liquid sample rules of thumb:
 - The closer to the first stage separator, the lighter it should be.
 - A higher RVP means a higher concentration of lighter hydrocarbons.
 - Separator samples should be near the bubble point.



Next slides show an example of an extended sample analysis.



Station Name: Station Number: Station Location: Sample Point: Meter Run Property ID: Sample Of:Natural GasSpotSample Date:05/23/2013Sample Conditions: 256 psig, @ 79 °FMethod:GPA 2286Cylinder No:1959Analyzed:05/24/2013 10:21:41 by LM

Analytical Data

| Analytical Bata | | | | | | |
|-----------------|---------|---------|----------------------|---------------|-------|--|
| Components | Mol. % | Wt. % | GPM at 14.73 psia | | | |
| Nitrogen | 0.985 | 1.347 | | GPM TOTAL C2+ | 5.013 | |
| Carbon Dioxide | 0.900 | 1.934 | | | | |
| Methane | 80.400 | 62.980 | | | | |
| Ethane | 11.104 | 16.303 | 2.979 | | | |
| Propane | 3.809 | 8.201 | 1.053 | | | |
| Iso-Butane | 0.700 | 1.987 | 0.230 | | | |
| n-Butane | 1.031 | 2.926 | 0.326 | | | |
| Iso-Pentane | 0.337 | 1.187 | 0.124 | | | |
| n-Pentane | 0.294 | 1.036 | 0.107 | | | |
| i-Hexanes | 0.122 | 0.507 | 0.051 | | | |
| n-Hexane | 0.073 | 0.302 | 0.030 | | | |
| Benzene | 0.004 | 0.013 | 0.001 | | | |
| Cyclohexane | 0.012 | 0.047 | 0.004 | | | |
| i-Heptanes | 0.069 | 0.323 | 0.030 | | | |
| n-Heptane | 0.025 | 0.117 | 0.011 | | | |
| Toluene | 0.009 | 0.040 | 0.003 | | | |
| i-Octanes | 0.048 | 0.263 | 0.024 | | | |
| n-Octane | 0.007 | 0.036 | 0.003 | | | |
| Ethylbenzene | 0.001 | 0.005 | 0.000 | | | |
| Xylenes | 0.008 | 0.042 | 0.003 | | | |
| i-Nonanes | 0.043 | 0.239 | 0.021 | | | |
| n-Nonane | 0.002 | 0.013 | 0.001 | | | |
| Decane Plus | 0.017 | 0.152 | 0.012 | | | |
| | 100.000 | 100.000 | 5.013 | | | |

| Station Name: | Sample Of: Natural Gas Spot | |
|-------------------------|--------------------------------------|----|
| Station Number | Sample Date: 05/23/2013 | |
| Station Location | Sample Conditions: 256 psig, @ 79 °F | |
| Sample Point: Meter Run | Method: GPA 2286 | |
| Property ID: | Cylinder No: 1959 | |
| | Analyzed: 05/24/2013 10:21:41 by I | LΜ |

| Physical Properties | Total | C10+ |
|--|------------------|--------|
| Calculated Molecular Weight | 20.48 | 137.95 |
| GPA 2172-09 Calculation: | | |
| Calculated Gross BTU per ft ³ @ 1 | 4.73 psia & 60°F | |
| Real Gas Dry BTU | 1216.1 | 7108.2 |
| Water Sat. Gas Base BTU | 1195.5076 | 6984.5 |
| Relative Density Real Gas | 0.7092 | 4.7626 |
| Compressibility Factor | 0.9966 | |



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Analyzing Data and Determining Emissions: Storage Tanks E&P TANK

- Next driver: separator pressure
 - The higher the separator pressure, the larger the pressure drop the separator liquid experiences when reaching the storage tank. This increases the potential for significant VOC emissions.
- Final driver: sales 'oil' RVP
 - The higher the RVP of the final liquid, the more volatile it is, and the higher the VOC emissions.
 - RVP 2 to 12 (higher RVP for shale wells, typically)
 - API Gravity 25 to 75 (higher API for shale wells, typically)



E&P TANK data inputs:

- Separator: pressure, temperature
- Known separator stream composition data.
 Options are listed in order of preference (details to follow):
 - Low pressure oil
 - High pressure oil
 - Low pressure gas



E&P TANK data inputs:

- Storage tank data only if AP-42 method is chosen for working and breathing losses
 - If RVP distillation method is chosen, tank data cannot be entered.
 - If AP-42 is chosen, ensure the tank location did not default to Homer, Alaska.

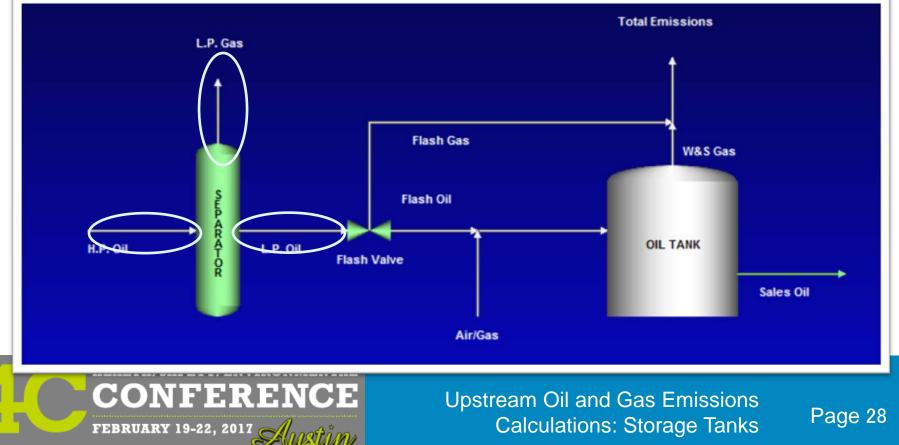


E&P TANK data inputs:

- Sales oil data:
 - production rate,
 - days of operation,
 - API gravity,
 - composition data,
 - RVP, and
 - bulk liquid temperature.



Ensure the actual sample analysis location matches the E&P TANK reported location:



Which separator stream option in E&P TANK should be used?

- Most preferred option is low pressure oil stream
 - Model is dealing with known data, not trying to predict stream composition after flash occurs at separator



Which separator stream option in E&P TANK should be used?

- Least preferred option for sweet gas sites is low pressure gas
 - Limited data on liquid inputted into the model, complicating emissions calculations
 - May be useful for sour gas sites, since hydrogen sulfide is more easily measured in the gas phase
 - Requires additional analyses to run model:
 - GOR analysis
 - Liquid sample analysis to obtain API gravity, RVP, and composition data for C7 to C10+ hydrocarbons



Let's analyze case study site values

- Start with gas analysis
- Move to E&P TANK report



Upstream Oil and Gas Emissions Calculations: Storage Tanks

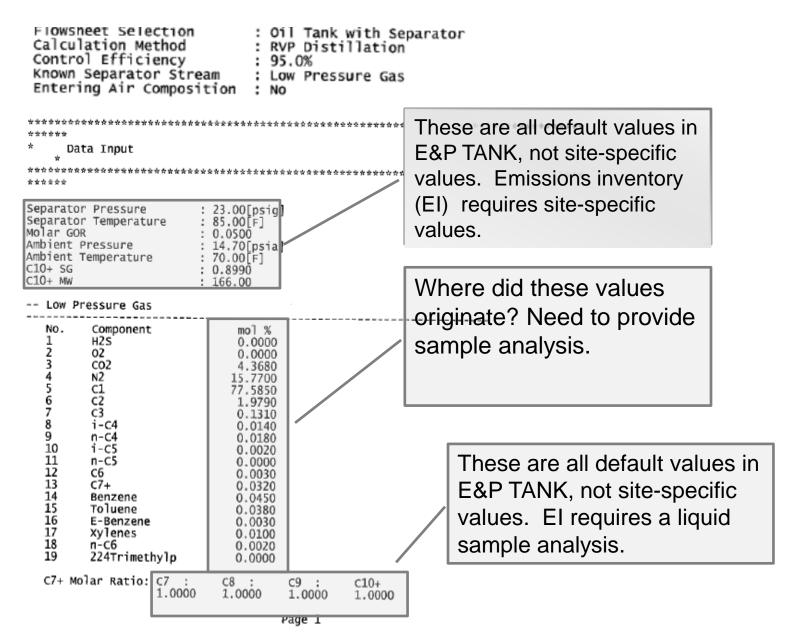
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Gas Analysis

| Conversion of Mole Per | cent to Weight I | Percent | | | High CO2 volume % |
|---|---------------------------------------|--------------|--|-----------|---|
| Specific Gravity | 0.5996 | | | | indicates this sample is |
| Gross BTU | 964 | | | | |
| e en gran agentar A estructura de la compositiva de la compositiva | · · · · · · · · · · · · · · · · · · · | nettorio Com | and a second | · · · · · | possibly untreated separator |
| A. Grand & Street | · · · · · · · · · · · · · · · · · · · | | Mole %* | | gas stream |
| Component | Mole % | MW | MW | Weight % | gas stream |
| Carbon Dioxi le | 3.3130 | 44 | 1.4577 | 8.429% | ii a |
| Nitrogen | 0.8170 | 28 | 0.2288 | 1.323% | 910 A |
| Hydrogen Sulfide | 0.0000 | 34 | 0.0000 | 0.000% | , # |
| Helium | 0.0000 | 4 | 0.0000 | 0.000% | |
| Methane | 94.3560 | 16 | 15.0970 | 87.298% | |
| Ethane | 1.3840 | 30 | 0.4152 | 2.401% | , N |
| Propane | 0.0680 | 44 | 0.0299 | 0.173% | These values ennear |
| so-Butane | 0.0040 | 58 | 0.0023 | 0.013% | These values appear |
| V-Butane | 0,0050 | 58 | 0.0029 | 0.017% | rounded (potentially by |
| so-Pentane | 0,0060 | 72 | 0.0043 | 0.025% | d P |
| N-Pentane | 0'0070 | 72 | 0.0050 | 0.029% | Excel). Duplication of 0.001 |
| Methylcyclopentane | 0.0000 | 86 | 0.0000 | 0.900% | values appears unusual. |
| h-Hexane | 0.0010 | 86 | 0.0009 | 0.005% | |
| Iexane + | 0.0000 | 86 | 0.0000 | 0.000% | |
| 2,4-Dimethylpentane | 0.0000 | 100 | 0.0000 | 0.000% | |
| Methycyclohexane | 0.0000 | .96 | 0.0000 | 0.000% | |
| Benzene | 0.0010 | 78 | 0.0008 | 0.005% | HEXANES |
| Cyclohexane | 0.0010 | 84 | 0.0008 | 0.005% | NMHC 0.5102 2.950% |
| -Heptane | 0,0010 | 100 | 0.0010 | 0.006% | VOCs (NMNEHC) 0.0950 0.549% |
| Coluene | 0.0010 | 92 | 0.0009 | 0.005% | HAPs 0.0057 0.03% |
| Ethylbenzene | 0.0000 | 106 | 0.0000 | 0.000% | H2S Mole Fraction 0.0000 0.000% |
| Kylenes | 0.0030 | 106 | 0.0032 | 0.018% | Total HC 15.6072 90.248% |
| Octanes+ | 0.0020 | 114 | 0.0023 | 0.013% | THC:VOC Ratio 0.6087 0.609% |
| Vonanes+ | 0.0140 | 128 | 0.0179 | 0.104% | ىلىغۇردۇر يەرەپەر ئۇرۇلۇرىلەر مىلاد مەرەپ مەرەپ مەرەپ يەرەپ بەرەپ بەرەپ بەرەپ بەرەپ بەرەپ بەرەپ بەرەپ بەرەپ بەر |
| Decanes+ | 0.0160 | 142 | 0.0227 | 0.131% | |
| [ota] | 100.000 | Ξ. | | 100.000% | |
| · · · · · · · · · · · · · · · · · · · | | | 314 kata 2 | | 2 |

Molecular Weight

E&P TANK Report



| E8 | P T | ANK | (Re | port | • |
|---|--|---|--|--|--|
| ****** * Calculation | re : 46.0 re : 7.70[*********************************** | days/year] psia] | **** | ************************************** | These are all default values in E&P TANK (except for the production data), not site- specific values. Reported emissions are potentially |
| Item Total HAPS Total HC VOCs, C2+ VOCs, C3+ | Uncontrolled [ton/yr] 2.333 0.549 0.399 | Uncontrolled [lb/hr] 0.005 0.533 0.125 0.091 | Controlled [ton/yr] 0.001 0.117 0.027 0.020 | Controlled [lb/hr] 0.000 0.027 0.006 0.005 | inaccurate. |
| Uncontrolled Recov Vapor HC Vapor GOR Emission Compos | 288.3300 x1E- 249.9200 x1E- 5.77 | 3 [MSCFD] 3 [MSCFD] [SCF/bb1] | | | |
| No Component 1 H2S 2 O2 3 CO2 4 N2 5 C1 6 C2 7 C3 8 i-C4 9 n-C4 10 i-C5 11 n-C5 12 C6 13 C7 14 C8 15 C9 16 C10+ 17 Benzene 18 Toluene 19 E-Benzene 20 Xylenes 21 n-C6 22 224Trimethylp Total | Uncontrolled [ton/yr] 0.000 0.000 0.411 0.256 1.783 0.151 0.016 0.002 0.003 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.237 0.086 0.033 0.001 0.009 0.008 0.001 0.009 0.008 0.001 0.002 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000 | Uncontrolled [lb/hr] 0.000 0.094 0.058 0.407 0.034 0.004 0.000 0.001 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.008 0.000 0.002 0.002 0.002 0.002 0.000 0.001 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000 | Controlled [ton/yr] 0.000 0.000 0.411 0.256 0.089 0.008 0.001 0.000 | Controlled [lb/hr] 0.000 0.004 0.058 0.020 0.002 0.000 | |
| Stream Data No. Component | MW | LP Oil Flas Page 2 | sh oil Sale Oil | Flash Gas W&S | Gas |

Questions?

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